

Outage Report for January 23-26, 2026 Cold Weather Event (M12694)
NSPI Responses to NSEB Information Requests

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1 **Request IR-1:**

2
3 **Reference page 6 of the report.**

4
5 **Please explain what “system adjustments” were implemented after the February 4, 2023,**
6 **extreme cold weather event.**

7
8 Response IR-1:

9
10 Figure 6 of the “Final Outage Report for February 3-5, 2023 Cold Weather Event” report (M10987)
11 confirms that all system adjustments identified during the February 4, 2023 event were addressed
12 and captured in the final report.

13
14 NS Power continues to maintain, improve, and implement its Cold Weather Preparedness Plan and
15 identifies vulnerable locations for improvement following each cold weather event. In addition,
16 NS Power continues to maintain Ligan 2 in a cold storage state in which the unit can be pivoted
17 to a recallable and operational state as cold weather / high load events are forecast.

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Request IR-2:

Reference page 7 of the report.

The report states that data from the February 4, 2023, event was used to “identify heavily loaded feeders which are subject to protective devices that could be at risk of tripping during extreme cold/load conditions.”

(a) How did the identified feeders perform in the January 2026 cold weather event?

(b) Please provide each feeder’s rated capacity identified as heavily loaded, as well as the peak load before and during the January 2026 cold weather event.

(c) To the extent that feeders tripped or were considered to be at risk of tripping in the January 2026 cold weather event and were not identified from the February 4, 2023 data, what factor(s) does NS Power attribute to other feeders that were not identified (if any) which tripped or were at risk of tripping in the most recent event?

Response IR-2:

(a) There were no reported outages during the January 23-25 2026 Cold Weather Event on devices that were identified as part of the preparation process arising from the February 4, 2023 event.

(b) The analysis identified heavily loaded protection devices (reclosers or breakers) by calculating a ratio of their most recently identified peak load (2025 peak model) and their minimum overcurrent trip setting. This criterion provided an indication of where abnormally high load could potentially cause an undesired trip and allowed NS Power to initiate mitigation measures ahead of the event. Mitigation measures included evaluation of protection changes, offloading load to an adjacent source, etc.

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In general, feeders have a design rating of 325 amps for regular loading, except in cases where derating is required due to thermal or other limitations. This criterion allows for emergency capacity during extreme cold weather, restoration, and other abnormal conditions.

The following feeders were identified as being at risk. Note that 16N-301 does not have real-time monitoring, and the actual loading during the January event is not available. This is also true for 92H-331; however, the loading was observed locally at the substation during the event.

Feeder	Protection Limit (A)	Normal Peak (A)	Jan 25 Peak (A)	Notes
92H-331	560	432	575	Protection setting was temporarily increased during the event to prevent tripping. Project C0083570, if approved, will address this overload.
103H-434	560	378	443	Project C0046358 will address this overload.
16N-301	400	322	N/A	Meter data will be used to model the peak load on this feeder during January 25, 2026. A long term solution is being prepared.

In addition to overall feeder protection, the same analysis was performed for all downline reclosers - over 1,500 devices in total. There were 27 devices identified by the analysis to be potentially at risk. Mitigation measures were implemented on these devices, and none of these 27 devices were reported to have operated during the event due to overload. Not all downline devices have real-time monitoring, so actual loading during the event will not be known until appropriate models are developed with AMI meter data. This analysis is underway now.

As noted in the Report, there was one device, 512N-311, that did experience tripping due to loading during the event. NS Power SMEs analyzed the device performance and a technician was deployed during the event to apply changes to the device settings in the

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1 field, resolving the issue. This device was originally missing from the list of at-risk devices
2 due to a modelling error. This error has since been resolved. Please see the response to IR-
3 12 for more details.

4
5 (c) None of these feeders experienced tripping due to overload during the January 2026 event
6 and there are no other feeders that were identified as at risk during the event.

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1 **Request IR-3:**

2
3 **Reference page 7 of the report.**

4
5 **With respect to the “substation transformers” and “bulk power substations or assets” that**
6 **were anticipated to be at risk for overload, how did the identified infrastructure perform in**
7 **the January 2026 cold weather event?**

8
9 Response IR-3:

10
11 Substation infrastructure performed as expected throughout the event with only one instance of
12 precautionary rotating outages initiated due to substation infrastructure overload concerns, as per
13 page 18 of the report. This precaution was addressed upon an inspection of equipment temperature
14 by a technician on site and an evaluation by a NS Power operations engineer. This same inspection
15 and evaluation methodology was employed to avoid additional outages on other identified
16 infrastructure that approached the threshold where rotating outages may have become necessary.

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Request IR-4:

Reference page 7 of the report.

“Select areas were identified across the Province where restoration is known to be subject to cold load pickup (very high loading following an outage) and plans were prepared by the Energy Delivery Services Regional Engineering team to streamline the restoration process, where possible.”

(a) How are these areas identified?

(b) Why would they be subject to cold load pickup?

Response IR-4:

(a) Winter peak loading on reclosers is monitored to identify locations where loading is high relative to the minimum trip setting. At these locations, additional sectionalizing points are required to enable restoration of feeder sections following extended outages during cold weather (cold load pickup). Detailed restoration plans are developed to guide crews on where to sectionalize feeders in order to minimize restoration time. Field personnel feedback is considered to supplement loading data, particularly in areas where past difficulties in restoring feeders or feeder sections have been experienced due to increased sensitivity to cold load pickup.

(b) Cold-load pickup is a loss of load diversity when circuits are re-energized following an extended outage during cold weather. The effect is temporary loading that exceeds normal peak loading by as much as 2-3 times. All feeders serving electric heating loads are susceptible to cold-load pickup. The feeders identified in this analysis are located in areas that have experienced significant electrification or population growth in recent

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1 years, increasing their loading relative to protection settings and sensitivity to cold-load
2 pickup conditions.

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1 **Request IR-5:**

2
3 **Reference page 8 of the report.**
4

5 **“NS Power maintains and implements its Cold Weather Preparedness plan as**
6 **outlined in the NERC Standard, EOP-012-2 “Extreme Cold Weather Preparedness**
7 **and Operations”. Planning and preparations for the severe weather and load events**
8 **were carried out in the week prior to the event with the focus on hardening the**
9 **generation fleet for the upcoming cold snap, topping up site fuel inventories,**
10 **optimizing generation output where possible, and staffing various sites for improved**
11 **response times.”**
12

13 **(a) The Board recently approved an updated version of the Extreme Cold Weather**
14 **Preparedness and Operations (EOP) standard. EOP-12-3 was approved on February**
15 **28, 2026, with an effective date of July 1, 2026. Please provide a status update**
16 **confirming that implementation remains on track for July 1, 2026.**
17

18 **Response IR-5:**
19

20 NS Power has reviewed the updated version of EOP-012-3 “Extreme Cold Weather Preparedness
21 and Operations” and as part of proceedings within M12577 provided its recommendations for
22 acceptance of the updated standard on January 16, 2026. Work to align NS Power’s internal
23 processes and procedures with the updated standard is already underway and NS Power anticipates
24 that remaining modifications to cold weather preparedness planning and any associated
25 compliance documentation will be completed in line with the effective date of the updated
26 standard.
27

28 **Key activities in progress include:**
29

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- 1 ○ Alignment of internal compliance documents to reflect changes to EOP-012-3, in
2 particular, updates to timelines for CAP extensions and submission of CAP
3 extensions and Generator Cold Weather Constraints to the Compliance
4 Enforcement Authority (CEA) for approval.
5
- 6 ○ Review of NS Power's Cold Weather Preparedness Plan for relevant updates such
7 as Calculated Extreme Cold Weather Temperature tracking
8
- 9 Training of responsible personnel as appropriate on these changes will occur prior to the effective
10 date of July 1, 2026.

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Request IR-6:

Reference page 9 of the report.

With respect to the Grid Status Index displayed on the web page:

- (a) Please explain the procedure that was used to review the status reported on the Index.
- (b) Was the Index reviewed at regular fixed time intervals for a potential change? If not, please explain how it was determined that the “status” of the grid status index should be confirmed or changed.

Response IR-6:

- (a) As the cold weather event approached, NS Power forecast that the system load and reserve margin could exceed the available generation. Additionally, based on analysis conducted with data collected during the February 2023 extreme cold event, impacts to transmission and distribution equipment were likely to occur when the total system load exceeded 2,250 MW. Based on the review of the load forecast and generation dispatch plan by the Control Centre Operations team, both capacity shortfalls and load exceeding 2,250 MW were anticipated starting Saturday, January 24. Accordingly, the decision was made to issue the “Warning” status on the morning of Saturday, January 24.
- (b) Leading up to and throughout the cold weather event, the Event Monitoring Team (which included NS Power Communications leads) met a minimum of twice a day to review and discuss all conditions related to the forecast, generation capacity, and impacts to transmission and distribution equipment, which are the determining factors of the Grid Status Index. The Index remained at the “Warning” level until Monday morning (January 26) when capacity shortfalls and load exceeding 2,300 MW were no longer anticipated based on the review of the load forecast and generation dispatch plan by the Control Centre

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1 Operations team. At that time, it was agreed that the Grid Status Index should be and was
2 adjusted to “Normal.”

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1 **Request IR-7:**

2
3 **Reference page 9 of the report.**

4
5 **“...Large Industrial Interruptible Rider (LIIR) customers were contacted by the Key**
6 **Accounts team on January 23, 2026...”**

7
8 **Reference page 14 of the report.**

9
10 **“To ensure operating reserves were maintained, the LIIR customers without data**
11 **telemetry and control were interrupted, providing an estimated 20 MW of load relief.**
12 **The LIIR customers with data telemetry and operator control were not interrupted**
13 **during the event,...”**

14
15 **(a) Please explain the substance of the January 23, 2026, LIIR customer contacts by the**
16 **Key Accounts team.**

17
18 **(b) Were all LIIR customers contacted or was it only those not equipped with telemetry**
19 **and control?**

20
21 **(c) Please provide the time that interruption notifications were issued, the time the**
22 **interruptions occurred, and the durations. If notifications were not issued, please**
23 **explain why not.**

24
25 **Response IR-7:**

26
27 **(a) The Key Accounts team reached out in advance to LIIR customers to provide notice of the**
28 **upcoming extreme cold event throughout the weekend and how NS Power was preparing**
29 **for this event across the province. The communications to the LIIR customers included the**
30 **following:**

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- Our teams are preparing for an extremely cold weekend across the province.
- Nova Scotia Power is treating this similar to other extreme weather events, with representatives from across the organization preparing the Power System for the upcoming weather.
- From Saturday evening through to Monday, temperatures could get as low as -21 degrees.
- This type of cold means significantly more demand for energy on the system from all customers.
- That's why our teams in power plants and in the field across the province have been planning ahead so they're prepared and ready to respond to this high demand for energy. We want to ensure the safety of our customers and the electricity grid.
- We will maximize our generation capacity, including our two new grid-scale battery sites, and electricity imports from our neighbouring utilities.
- The system will be tight all weekend.
- We do know that the potential to interrupt our customers is high for both LIIR non-telemetry and LIIR telemetry, with the largest risk occurring Sunday evening after 5PM.
- As always, this is subject to change, and we will communicate via our normal channels. We wanted to share this information ahead of time to help with your weekend planning.

(b) All LIIR customers were contacted.

(c) The interruptions times issued from the outbound call system are noted in the table below as shown in Figure 8 on page 15 of the event report. The duration of the requested interruption, based on these call times, was 317 minutes. When customers receive the interruptions notifications, they must shed the entire interruptible portion of their load within 10 minutes.

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1

Interruptible Industrial Notifications	Call Time
Advisory LIIR	25-Jan-26 @ 16:15
Alert LIIR	25-Jan-26 @ 16:17
Advisory LIIR Telemetry and Control	25-Jan-26 @ 16:18
Interruption LIIR Non-Telemetry and Control	25-Jan-26 @ 16:47
Alert LIIR Telemetry and Control	25-Jan-26 @ 16:49
RESTORE LIIR Non-Telemetry and Control	25-Jan-26 @ 22:04
Alert Cancellation LIIR Telemetry and Control	25-Jan-26 @ 22:19
Alert Cancellation LIIR	25-Jan-26 @ 22:19
Advisory Cancellation LIIR Telemetry and Control	25-Jan-26 @ 22:21
Advisory Cancellation LIIR	25-Jan-26 @ 22:21

2

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1 **Request IR-8:**

2
3 **Reference page 13, Figure 5, of the report.**

4
5 **The table shows peak Maritime Link imports of just over 250 megawatts in the early**
6 **evening hours of January 25, 2026. Given the recent positive test on the Labrador Island**
7 **Link operating at 900 megawatts, please provide an estimate of the Maritime Link imports**
8 **that could be expected in the future events, assuming similar conditions to that which existed**
9 **on January 25, 2026. Would the increased capacity of the Labrador Island Link of 900**
10 **megawatts increase the reserve capacity on NS Power's system in similar conditions?**

11
12 **Response IR-8:**

13
14 The Labrador Island Link (LIL) is currently operating with a maximum flow of 700 MW. The
15 recent positive results of the high-poer tests on the LIL will allow for future increased flows over
16 the LIL, once accepted by the Newfoundland System Operator. Increased imports to Nova Scotia
17 from Newfoundland and Labrador, while theoretically possible up to the limit of the Maritime
18 Link (475 MW), would depend on many factors including the actual generation availability, load
19 in the province of Newfoundland and Labrador, and prevailing market conditions. Consequently,
20 it is not currently possible to provide an estimate of available imports and timing of availability.

21
22 No, the increased capacity of the LIL would not increase the reserve capacity on NS Power's
23 system, because assets on Newfoundland's bulk power system do not increase or decrease Nova
24 Scotia Power's system reserves.

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Request IR-9:

Reference page 17 of the report.

“Pre-event, NS Power’s operational power system engineers, with support from the planning team at the Independent Energy System Operator – Nova Scotia (IESO-NS), re-studied stability limits with the addition of new transmission-connected Battery Energy Storage Systems (BESS) and increased the Onslow South Corridor limit by 45 MW.”

(a) How was this new limit established? Is it based on the storage capacity of the two operational BESS projects (combined output of 100 MW for 4 hrs)?

(b) Please explain how the battery charging is planned, and how and when their energy is dispatched?

Response IR-9:

(a) The Onslow South transmission corridor transfer limit is governed by electrical grid operating constraints including voltage stability limits during winter conditions and thermal limits during summer conditions. Consequently, this limit is determined by the reactive power and voltage support capability of the BESS sites rather than by the energy storage capacity (MWh) of the BESS sites. Each BESS installation provides up to ± 45.3 MVar of reactive power capability. This reactive capability is independent of the real power (MW) output of the BESS and can be fully utilized irrespective of charging or discharging status, subject to inverter limits.

(b) The day-ahead charging and discharging of BESS sites falls under the responsibility of the NS Power Marketing group. The NSPSO is responsible for ensuring that adequate generation is planned for day-ahead to ensure the electrical system can operate reliably.

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1 During the cold event of January 23-25, 2026, the NSPSO ensured that both BESS sites
2 were fully charged ahead of the forecast cold load. The NSPSO dispatches all available
3 energy resources including the BESS sites as per the Capacity and Energy Emergency
4 Procedure during extreme cold events

5
6 During the cold weather event, the NSPSO utilized both the reactive power capability of
7 the BESS and available capacity support to maintain system reliability. Specifically, the
8 Spider Lake BESS was injecting approximately 33 MVAR, while the Bridgewater BESS
9 was injecting approximately 17 MVAR during the event.

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Request IR-10:

Reference page 18 of the report.

70W High Street “Rotating feeder outages were initiated at 70W High Street to avoid overload conditions reaching the protection limit for transmission line L-5545:” ... “At 10:41, it was confirmed that the protection limit was increased on L-5545 and rotating outages were cancelled.”

Reference page 22 of the report.

“The long-term resolution to the L-5545 overloading issue is a proposed new substation which will offload the transmission line.” Also, protection settings were reviewed and adjusted after the 2023 event.

(a) Please provide the present rated loading capacity of Transmission Line L-5545, as well as the loading expressed as a percentage of the rated capacity during the January weather event, along with the actual values reached during the January cold-weather event.

(b) What temporary solutions are available to avoid rotating feeder outages in the event of another transmission-line overload?

(c) When did the utility first identify the transmission-line loading issue, and since that date, what action was taken to avoid rotating feeder outages?

(d) What protection settings were changed? Please provide the values that were modified in 2023, the new settings, and the maximum allowable values.

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1 Response IR-10:

2
3 (a) The “cold season” overload limit for transmission line L-5545 is 64 MVA. On January 25
4 2026, the transmission line reached 54.3 MVA (84 percent of the limit).

5
6 (b) To reduce the risk of rotating outages in the event of future asset overload conditions,
7 several temporary measures that can be implemented, including proactive load transfers to
8 adjacent distribution sources, the application of modified operating limits during extreme
9 cold weather, and enhanced local monitoring at locations where SCADA is not available.

10
11 (c) This issue was identified during the February 3-5, 2023 Extreme Cold Event and it was
12 subsequently corrected by increasing the protection limit. This was further updated during
13 the January 23-25, 2026 Extreme Cold Event by updating the SCADA alarm to the revised
14 protection limit. The increase in protection limit and SCADA alarm to 64 MVA addresses
15 the near-term load growth at this substation until a new substation is in service. A
16 distribution planning study is ongoing to address overload issues permanently.

17
18 (d) The following table summarizes the settings that were changed resulting in increasing the
19 capacity of transmission line L-5545. The line is protected via overcurrent relays and this
20 current value can be translated to a power rating in MVA as the voltage is near constant.
21 The protection settings are determined by short circuit study, and a lower setting will result
22 in faster fault clearing. The settings can be increased to a maximum current that translates
23 to 128 MVA while still aligning with acceptable industry practice for clearing times and
24 fault detection. Prior to the 2023 cold event the protection setting was 57 MVA, and
25 subsequent study following the event determined an ideal setpoint between line loading
26 and protection sensitivity was 64 MVA and was increased accordingly. This setting
27 remains at 64 MVA after the 2026 cold event. The SCADA alarm prompting the operator
28 to take immediate action prior to hitting the trip limit was reviewed post 2026 cold event
29 and was corrected to reflect the post 2023 cold event protection limit.

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1

Cold Season Rating	Protection Limit	SCADA Alarm Limit
Post 2023 Cold Event	64 MVA	54 MVA
Post 2026 Cold Event	64 MVA	61MVA

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Request IR-11:

Reference page 18 of the report.

79V Three-Mile Plain “Loading above design limit was observed on transformer 79V-T1 Rotating feeder outages were initiated to protect the asset until the winding temperature could be verified in the field.” ... “A technician arrived on site at the substation and confirmed that the winding temperature was within acceptable limits and the rotating outages were cancelled.”

(a) Is there any remote monitoring (SCADA) available at 79V, or must a technician be on site to confirm the winding temperature?

(b) Please provide the transformer’s rated capacity, its allowable winter loading capacity, and the actual loading observed during the January cold-weather event.

(c) Please explain the relationship between loading above design limits and transformer winding temperatures. Additionally, clarify why the field technician’s confirmation that the winding temperature was within acceptable limits indicates that the transformer was not overloaded.

Response IR-11:

(a) SCADA is available at Substation 79V; however, the transformer is not equipped with a monitor that provides real-time winding temperatures through SCADA. As a result, confirmation of actual winding temperature on the transformer during the event required a field technician to travel to the substation and take local measurements.

**(b) Transformer rated capacity: 28 MVA.
Allowable winter-loading capacity: 37.5 MVA (133 percent).**

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1 Maximum actual load observed during the event: 39.3 MVA.

- 2
- 3 (c) A transformer's thermal design limit is governed by its ability to dissipate heat generated
4 by electrical losses while maintaining conductor and insulation temperatures within
5 acceptable limits that avoid excessive insulation damage. Transformer nameplate ratings
6 are established assuming a reference ambient temperature of 30 °C and an allowable
7 winding temperature rise of approximately 65 °C above ambient, corresponding to a
8 nominal maximum winding temperature of approximately 95 °C.

9

10 When ambient temperatures are significantly below this reference value — as occurred
11 during the January cold weather event — the transformer's ability to dissipate heat is
12 materially improved. Under these conditions, higher electrical loading can be
13 accommodated without exceeding acceptable winding temperature limits. This enhanced
14 capability is explicitly reflected in NS Power's established cold-weather and emergency
15 loading ratings.

16

17 In this context, the term "overloaded" refers strictly to loading above the transformer's
18 nameplate rating, which is based on conservative thermal assumptions rather than real-time
19 operating conditions. While the observed load of 39.3 MVA exceeded the nameplate
20 rating, it remained within a range that could be safely managed given the prevailing cold
21 ambient temperatures.

22

23 The field technician's confirmation that winding temperatures were within acceptable
24 limits demonstrated that the transformer was not experiencing excessive thermal stress,
25 accelerated loss of life, or risk of insulation damage at the time. Based on this information,
26 NS Power engineering staff determined that continued operation at this level of loading
27 would not compromise asset integrity.

28

29 Accordingly, the decision to cancel the rotating feeder outages was supported by:

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- 1 • the very low ambient temperatures during the event, which increased the
- 2 transformer's thermal margin;
- 3 • direct verification that winding temperatures remained within acceptable limits; and
- 4 • load forecasts indicating that customer demand would not continue to rise to levels
- 5 that could cause winding temperatures to approach a condition of concern.

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1 **Request IR-12:**

2
3 **Reference page 19 of the report.**
4

5 **“There was one reported case of repeated outages on downline recloser 512N-311,**
6 **located in the community of Hedgeville, Pictou County. The recloser tripped and**
7 **reclosed 18 times during the morning of January 25, affecting approximately 324**
8 **customers. The Engineering team analyzed the device performance, and a technician**
9 **was deployed to apply changes to the device settings in the field, resolving the issue.”**
10

11 **(a) What protection settings were changed? Please provide the values that were modified,**
12 **the new settings, and the reasons for the changes.**
13

14 **(b) How was the effectiveness of the new settings measured?**
15

16 **(c) Why were these settings not changed earlier?**
17

18 **(d) How does the utility determine which settings will be applied to each recloser?**
19

20 **(e) Is this a permanent solution to this problem on this line?**
21

22 **Response IR-12:**
23

24 **(a) The minimum pickup for phase overcurrent at the 512N-311 recloser was changed from**
25 **120 amps to 140 amps during the cold weather event, to accommodate loading that was**
26 **reaching 120 amps. There is no real-time monitoring available at this device, but the normal**
27 **peak load at this device is estimated to be approximately 90 amps.**
28

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- 1 (b) The new settings were designed and applied based on the measured load and modelled fault
2 levels. Following the revisions, load was observed and remained below levels that would
3 be at risk for tripping.
4
- 5 (c) Not all downline distribution devices have real-time monitoring. Evaluation of peak
6 loading is dependent on manual inspections that might not capture absolute peak periods
7 and development of peak load models using customer meter data. This device was not
8 originally flagged on the at-risk list due to a modelling error. This error has now been
9 corrected.
10
- 11 (d) Overcurrent protection for downline reclosers is designed such that the device can carry
12 the expected downstream peak load and also detect and clear a fault caused at the extent of
13 the protection zone (minimum fault level).
14
- 15 (e) This was a permanent solution that will be effective for near-term load magnitudes. Should
16 load increase, distribution line upgrades may be required in the future.

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1 **Request IR-13:**

2
3 **Reference page 19 of the report.**

4
5 **“On January 24th and 25th Tufts Cove 6 was derated for periods of time due to**
6 **freezing instrumentation tubing for a transmitter. An exterior wall mounted heater**
7 **was repositioned which resolved the issue. On January 25th Burnside 2 failed to start**
8 **due to a fuel control light off setting that required adjustment. The unit was**
9 **operational the following morning.”**

10
11 **(a) Did either of these events impact the need to interrupt the LIIR customers between**
12 **16:47 and 22:04 on January 25?**

13
14 **Response IR-13:**

15
16 On January 25, 2026 during the period of the non-telemetry LIIR customer interruption, Tufts
17 Cove 6 had already returned to service and was providing 45 MW to the grid. The Burnside 2
18 turbine was not available during that period. The additional 30 MW that Burnside 2 would have
19 provided if it was available would not have been enough additional capacity to prevent the non-
20 telemetry LIIR customer interruption. NS Power’s ten-minute reserve dropped to 140 MW below
21 the required level, so even with all available generation resources in use, and load management in
22 effect (non-telemetry LIIR customer interruption), emergency energy assistance of 130 MW from
23 neighbouring utilities was still required during this period.

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1 **Request IR-14:**

2
3 **Reference page 20 of the report.**

4
5 **“Wind generation tracked the forecast trend well. The January 24 day-ahead**
6 **forecast predicted a steeper generation decline than the two-day-ahead planning**
7 **forecast on January 23 as shown on the graph below, with the actual wind generation**
8 **dropping by 367 MW between the first and last hour of the day due to declining wind**
9 **speeds.”**

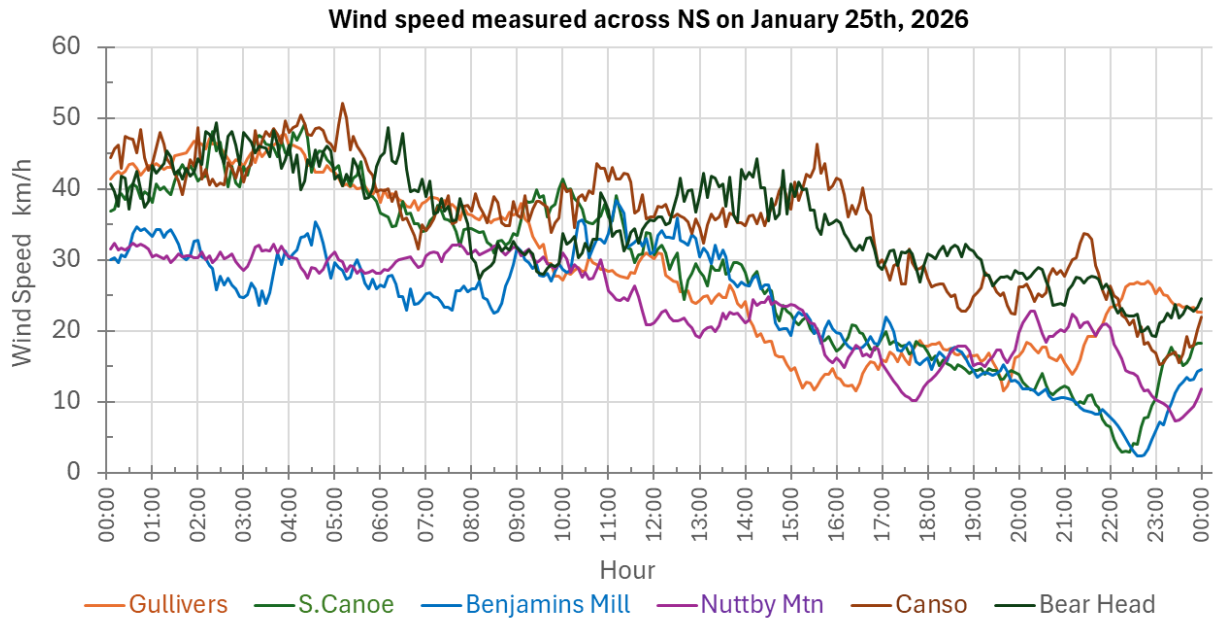
10
11 **(a) Please confirm whether there were any operational issues with the wind turbines, and**
12 **whether the low wind production on January 25 during the cold-weather event was**
13 **due to low wind conditions.**

14
15 **Response IR-14:**

16
17 No operational issues with the wind turbines were noted due to the January 23-26, 2026 cold
18 weather event. There was initial concern that there may be diminished output from certain turbine
19 models that can begin to occur when ambient temperatures drop below -15°C; however, this did
20 not occur. The decline in wind generation throughout the day was primarily due to decreasing
21 wind speeds across the province and is indicated in the wind speed chart for major wind farms
22 below.

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1

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Request IR-15:

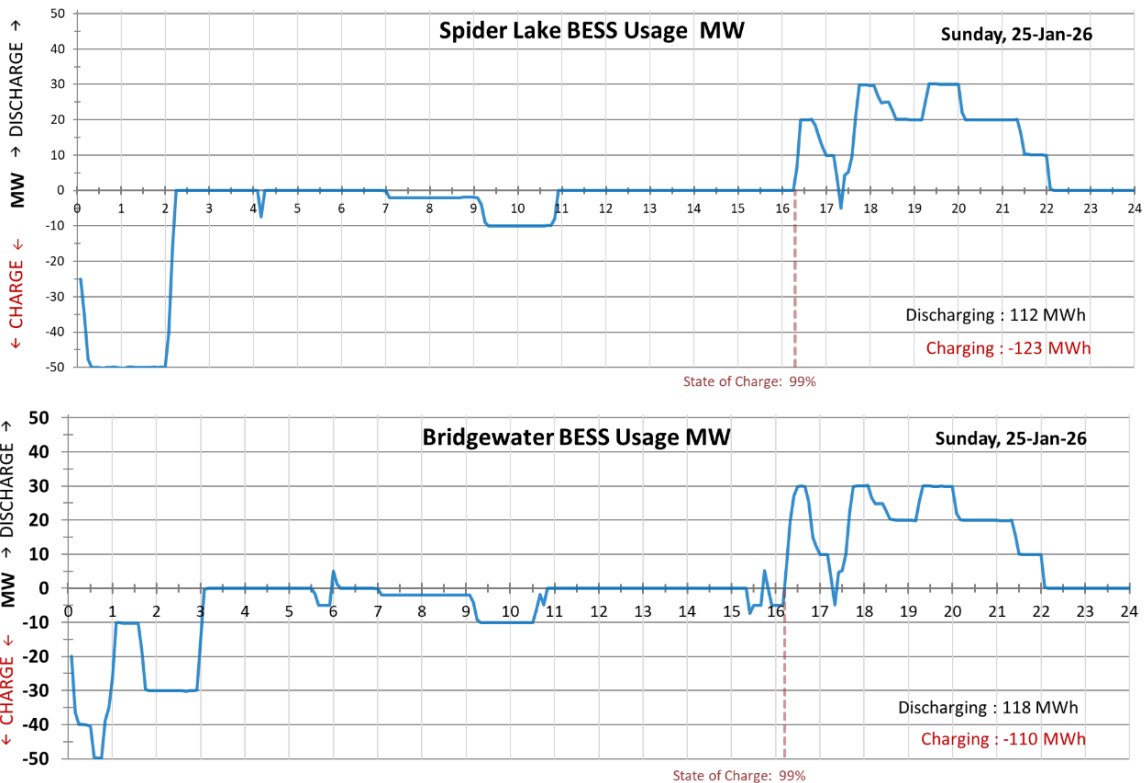
Reference page 21, Figure 13, Grid Battery Usage, of the report.

(a) Please provide similar separate tables for each of the two respective battery storage sites.

(b) Please explain the reason for the difference (if any) in the performance of the respective battery storage sites.

Response IR-15:

(a)



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1 (b) Both BESS sites performed well during the January 23-26 Cold weather event. As shown
2 in the above graphs, both sites were fully charged and available for the January 25 evening
3 peak. Each site is designed with a 50 MW capacity for a four-hour duration, resulting in
4 200 MWh capacity at each site., Both sites have identical configurations and demonstrated
5 similar behaviour, as expected. Over the course of the January 25 evening peak, the 132H-
6 Spider Lake BESS provided 112 MWh and the 99W-Bridgewater BESS provided 118
7 MWh energy to support customer load. Both sites were reduced to “0” MW output by the
8 Energy System Operator after the peak was over, and the BESS support was no longer
9 required to support load.

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Request IR-16:

Page 20 of 23, Figures 11 and 12 provide hourly average wind generation and forecasts.

(a) Please confirm whether the generation forecast was adjusted for cold weather.

(i) If not, please provide Figure 11 and Figure 12 with unadjusted and cold adjusted forecast.

Response IR-16:

A temperature-adjusted generation forecast was not prepared for this event.

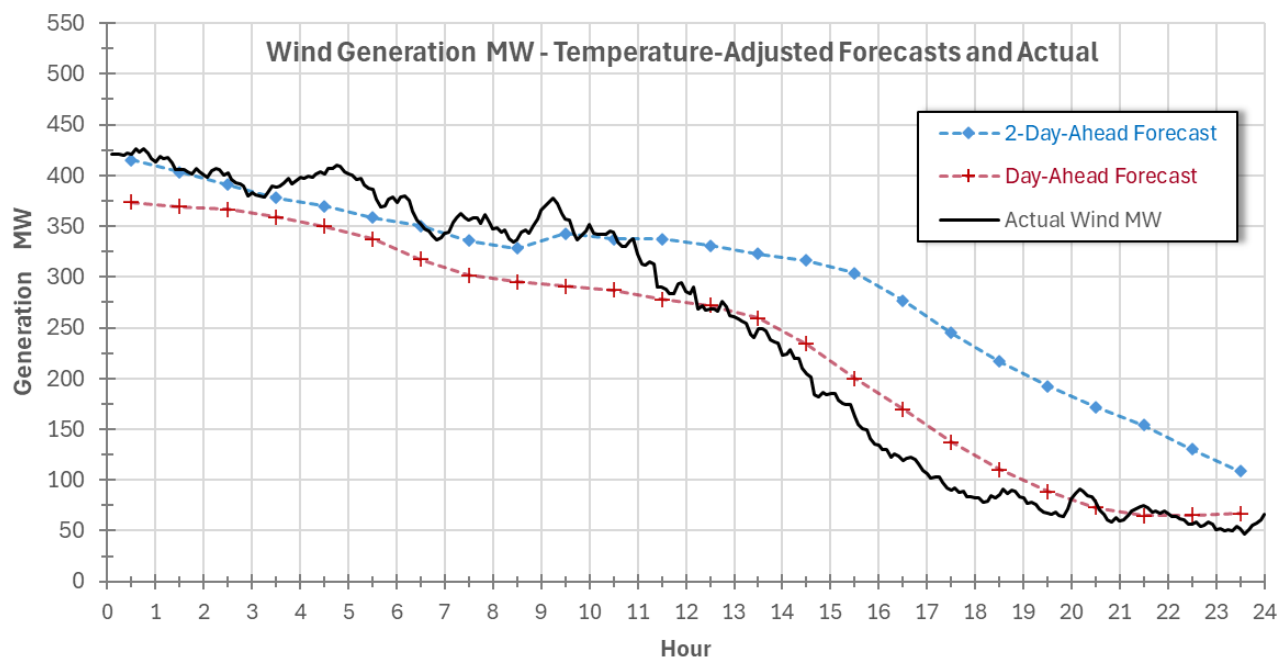
The turbines at some Nova Scotia wind farms without a Cold Weather Package in place may have diminished output when temperatures drop substantially below -15°C. Unlike the cold weather event of February 2023 when temperatures were in the -25°C range across much of the province, the temperatures forecast for the January 2026 event were expected to be between -15°C and -20°C for the high load periods of the day, so a reduction in wind generation output was not anticipated. Since a temperature-adjusted generation forecast was not prepared prior to the event, NS Power has reconstructed a forecast based on the available weather data, presented below.

January 25 Hourly Average Wind Generation and Temperature Adjusted Forecasts

Hour-ending:	1	2	3	4	5	6	7	8	9	10	11	12
2 Day-Ahead Forecast	415	403	391	378	370	358	350	336	328	343	337	337
Day-Ahead Forecast	374	369	366	359	350	337	318	301	295	291	287	278
Actual Generation MW	421	408	396	389	403	384	355	355	346	357	338	297
Hour-ending:	13	14	15	16	17	18	19	20	21	22	23	24
2 Day-Ahead Forecast	331	323	316	304	277	245	217	192	172	154	130	109
Day-Ahead Forecast	272	260	234	200	170	137	110	89	73	65	65	67
Actual Generation MW	271	244	202	159	120	92	84	71	74	69	58	54

Outage Report for January 23-26, 2026 Cold Weather Event (M12694)
NSPI Responses to NSEB Information Requests

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1

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Request IR-17:

- (a) Please provide the hourly load forecasts the utility prepared in advance of the January weather forecast that were used for generation dispatch planning.**
- (b) Referencing the hourly net load in Figure 5 of the report, please provide a list of the generation resources that supplied that net load during each hour and their rated capacity.**
- (c) Please provide a list of power generation resources that did not come online despite being required.**
- (d) Please provide a graph, along with the underlying data in an Excel spreadsheet, showing the hourly net load for January 24 and 25, 2026, the MW supply by resource for each hour, and the remaining generation (supply) available to the utility.**

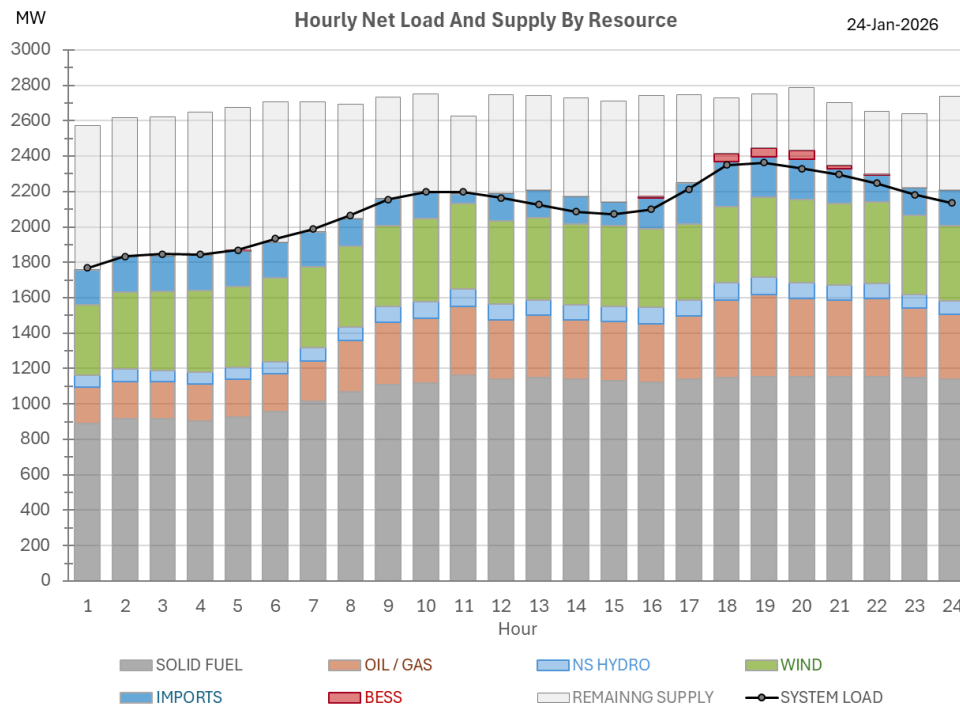
Response IR-17:

- (a) The hourly system dispatch plan for January 25, 2026 is provided in Attachment 1. Hourly load forecast is shown in the second column.**
- (b) The net generation and scheduled supply resources are provided in hourly system dispatch plans in Attachment 1. The plans were prepared on Friday January 23, 2026 when the status of available energy from Newfoundland was still uncertain due to the impacts from the Bay d'Espoir hydro plant icing issue, so only the Nova Scotia Block energy from Newfoundland is shown in this plan. The capacities of Tufts Cove units 4, 5, and 6 are combined under the heading "TUC6."**
- (c) The following are units that were delayed coming online despite being recalled during the January 23-26, 2026 cold weather event.**

Outage Report for January 23-26, 2026 Cold Weather Event (M12694)
NSPI Responses to NSEB Information Requests

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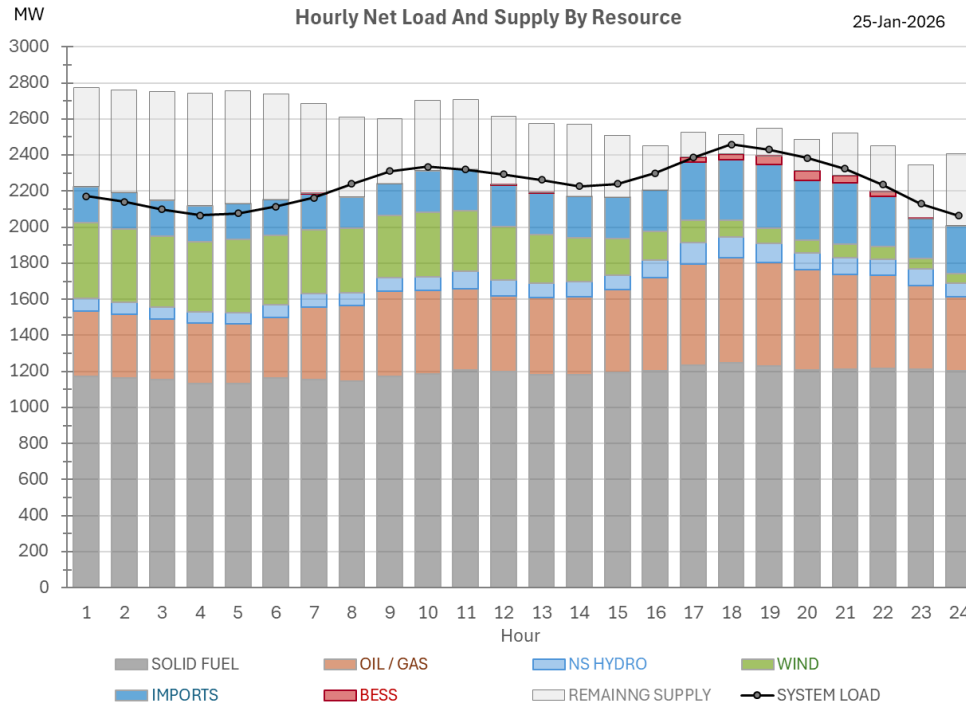
- a. Burnside 1 failed to start at 13:10 on January 23, 2026 and was made available again at 13:31 on the same day.
- b. Burnside 2 failed to start at 12:07 on January 25, 2026 and was made available again at 9:13 on January 26, 2026.
- (d) The graphs below show the system load and available supply by resource. The underlying data and individual generator details can be found in Attachment 2. The hourly remaining supply and reserves are indicated as the light grey bars at the top of the generation stack. Note that the generation appears higher than the NS system load for some hours of January 24 and the first 7 hours of January 25 because NS was providing emergency energy assistance to Newfoundland during those periods.



Outage Report for January 23-26, 2026 Cold Weather Event (M12694)
NSPI Responses to NSEB Information Requests

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2

Nova Scotia Generation Dispatch Data

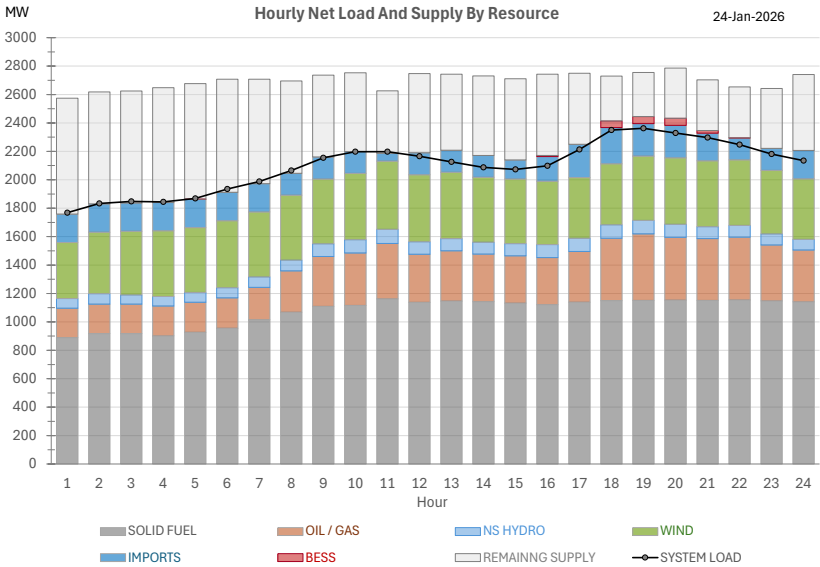
Date: Sat January 24, 2026

HOUR	LOAD FORECAST	RESERVE REQMT	SYSTEM MARGIN	PA1	LIN1	LIN2	LIN3	LIN4	TR5	TR6	PT2	TUC1	TUC2	TUC3	TUC6	CT TOTAL	IPP TOTAL	PT BIO	HYDRO TOTAL	BESS	WIND TOTAL	FIRM NB PURCH	FIRM NFD PURCH
1	1762	218	434	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	274	0	199
2	1748	218	488	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	315	0	199
3	1746	218	539	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	363	0	199
4	1762	218	542	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	382	0	199
5	1790	218	547	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	415	0	199
6	1849	218	506	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	433	0	199
7	1945	218	422	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	445	0	199
8	2041	218	286	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	450	0	154
9	2115	218	279	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	50	467	0	154
10	2153	218	247	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	50	473	0	154
11	2152	218	250	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	50	475	0	154
12	2141	218	261	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	50	475	0	154
13	2117	218	232	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	472	0	154
14	2096	218	248	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	467	0	154
15	2095	218	242	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	461	0	154
16	2139	218	235	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	457	40	154
17	2241	218	211	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	20	455	100	154
18	2356	218	174	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	100	453	100	154
19	2342	218	158	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	97	451	75	154
20	2305	218	164	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	60	457	75	154
21	2259	218	171	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	50	463	40	154
22	2201	218	193	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	50	467	0	154
23	2124	218	213	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	460	0	154
24	2043	218	331	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	452	0	199

Nova Scotia Generation Dispatch Data

Date: Sun January 25, 2026

HOUR	LOAD FORECAST	RESERVE REQMT	SYSTEM MARGIN	PA1	LIN1	LIN2	LIN3	LIN4	TR5	TR6	PT2	TUC1	TUC2	TUC3	TUC6	CT TOTAL	IPP TOTAL	PT BIO	HYDRO TOTAL	BESS	WIND TOTAL	FIRM NB PURCH	FIRM NFLD PURCH
1	2021	218	344	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	443	0	199
2	2004	218	351	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	433	0	199
3	2013	218	332	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	423	0	199
4	2025	218	309	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	412	0	199
5	2041	218	287	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	406	0	199
6	2085	218	233	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	396	0	199
7	2166	218	145	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	389	0	199
8	2239	218	119	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	30	376	75	154
9	2266	218	100	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	50	364	75	154
10	2271	218	104	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	50	373	75	154
11	2247	218	117	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	50	362	75	154
12	2213	218	116	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	20	357	75	154
13	2166	218	132	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	346	75	154
14	2123	218	162	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	333	75	154
15	2103	218	172	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	323	75	154
16	2129	218	132	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	309	75	154
17	2225	218	58	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	50	281	75	154
18	2352	218	-53	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	100	248	75	154
19	2378	218	-107	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	100	219	75	154
20	2357	218	-111	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	100	194	75	154
21	2287	218	-162	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	173	75	154
22	2221	218	-114	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	155	75	154
23	2128	218	-45	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	131	75	154
24	2022	218	84	165	148	142	142	140	85	148	151	75	85	125	139	192	25	30	149	0	109	75	199



Net Generation

Hour	System Load	PA1	LI1	LI2	LI3	LI4	TR5	TR6	PT2	TUC1	TUC2	TUC3	TUC4	TUC5	TUC6	BS1	BS2	BS3	BS4	VJ1	VJ2	TK4	IPP TOTAL	PT BIO	Small Hydro	WC1	WC2	Spider BESS	BW BESS	WIND TOTAL	FIRM NB PURCH	FIRM NFLD PURCH	NB/PEI Emerg Assist	NFLD Emerg Assist
1	1768	136	123	0	152	147	93	116	117	47	10	66	33	33	19	0	0	0	0	0	0	0	-8	13	56	0	0	-4	-25	395	0	199	0	0
2	1834	139	135	0	152	138	94	115	134	47	12	66	33	31	18	0	0	0	0	0	0	0	-8	19	55	0	0	-25	-25	433	0	199	0	0
3	1848	157	132	0	152	140	94	116	125	47	14	66	31	31	18	0	0	0	0	-1	0	0	-8	11	54	0	0	-25	-19	448	0	199	0	0
4	1844	154	120	8	148	141	93	116	119	47	17	66	32	31	18	0	0	0	0	-1	0	0	-8	12	56	0	0	-18	0	463	0	199	0	0
5	1869	147	112	42	151	147	92	116	116	47	19	66	31	31	17	0	0	0	0	-1	0	0	-9	12	58	0	0	0	0	456	0	199	0	0
6	1935	136	126	56	152	147	91	116	127	47	21	66	33	31	18	0	0	0	0	-1	0	0	-9	13	58	0	0	0	0	472	0	199	0	0
7	1988	136	137	71	151	148	87	140	140	48	23	66	37	35	19	0	0	0	0	0	0	0	-9	15	59	0	0	0	0	457	0	199	0	0
8	2066	137	138	101	152	147	97	148	141	70	26	81	46	45	24	0	0	0	0	0	0	0	-9	16	60	0	0	-1	0	457	0	154	0	0
9	2155	136	133	129	152	147	117	148	126	75	33	105	48	48	42	0	0	0	0	0	0	0	-9	29	61	0	0	-1	0	457	0	154	0	0
10	2197	137	134	135	152	147	120	149	122	75	50	103	48	48	46	0	0	0	0	0	0	0	-9	29	64	0	0	0	0	467	0	154	0	0
11	2198	156	138	138	151	147	119	151	142	75	56	123	47	47	43	0	0	0	0	0	0	0	-9	30	70	43	0	0	0	480	0	55	0	0
12	2165	161	118	135	151	147	118	151	147	61	75	106	39	39	18	0	0	0	0	0	0	0	-9	18	70	2	0	0	0	472	0	154	0	0
13	2126	161	137	135	150	146	119	151	140	53	89	120	37	36	18	0	0	0	0	0	0	0	-9	16	70	0	0	0	0	467	0	154	0	0
14	2087	162	147	132	151	147	116	151	131	49	85	123	32	31	15	0	0	0	0	0	0	0	-9	15	69	0	0	0	0	457	0	154	0	0
15	2073	161	148	133	152	147	108	151	126	49	74	115	43	43	10	0	0	0	0	0	0	0	-9	17	69	0	0	-1	0	455	-20	154	0	0
16	2099	161	148	133	147	147	102	151	124	49	71	111	45	45	10	0	0	0	0	0	0	0	-9	18	74	0	0	8	0	446	20	154	0	0
17	2213	161	149	133	154	147	103	151	136	49	80	123	44	42	19	0	0	0	0	0	0	0	-10	16	76	32	0	0	0	427	80	154	0	0
18	2350	161	148	131	155	146	97	151	151	71	89	128	48	48	21	16	0	15	0	2	0	0	-10	19	77	78	0	23	24	429	100	154	0	0
19	2362	161	151	131	152	147	98	149	153	74	91	128	48	48	20	18	0	19	0	21	0	0	-10	18	77	50	0	25	25	452	75	154	0	0
20	2329	161	151	130	148	147	107	149	153	74	92	128	48	48	24	17	0	6	0	5	0	0	-10	16	76	32	0	25	25	468	75	154	0	0
21	2297	161	152	128	142	145	115	149	153	74	95	128	48	48	24	17	0	0	0	0	0	0	-10	16	68	76	0	10	9	464	40	154	0	0
22	2247	161	151	129	144	143	115	149	153	74	96	128	48	48	24	24	0	0	0	0	0	0	-10	17	66	84	0	0	0	461	0	154	0	0
23	2181	161	150	127	145	142	115	150	154	55	96	128	44	47	23	-1	0	0	0	0	0	0	-13	16	62	80	0	0	0	447	0	154	0	0
24	2135	161	151	127	148	142	114	151	154	46	96	128	37	38	20	0	0	0	0	0	0	0	-20	16	60	6	0	0	-7	427	0	199	0	0

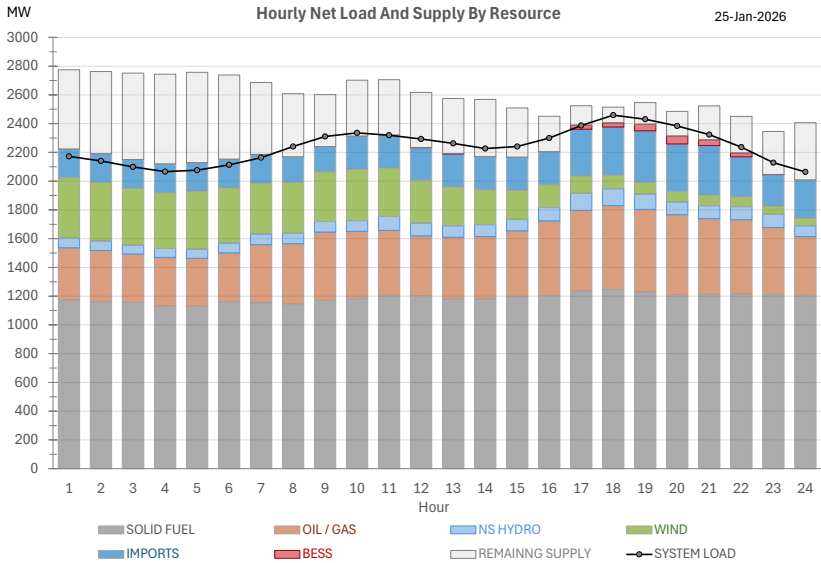
Chart Data

SOLID FUEL	OIL / GAS	NS HYDRO	WIND	IMPORTS	BESS Discharging
889	206	68	395	199	0
918	206	74	433	199	0
918	206	65	448	199	0
902	209	67	463	199	0
927	210	70	456	199	0
955	214	71	472	199	0
1016	227	74	457	199	0
1068	291	76	457	154	0
1109	351	89	457	154	0
1115	369	93	467	154	0
1162	389	100	480	55	0
1138	337	88	472	154	0
1147	353	86	467	154	0
1142	335	84	457	154	0
1132	333	86	455	134	0
1121	331	92	446	174	8
1139	357	93	427	234	0
1150	438	96	429	254	47
1151	468	95	452	229	50
1153	441	91	468	229	50
1151	434	84	464	194	19
1154	442	83	461	154	0
1148	392	79	447	154	0
1142	364	75	427	199	0

Max Net Output: 173 152 138 155 148 137 151 154 75 99 128 48 48 46 30 0 30 30 27 0 26 -8 41 77 100 0 50 50

Remaining Generation Supply / Reserve

Hour	REMAINING SUPPLY /RESERVE	PA1	LI1	LI2	LI3	LI4	TR5	TR6	PT2	TUC1	TUC2	TUC3	TUC4	TUC5	TUC6	BS1	BS2	BS3	BS4	VJ1	VJ2	TK4	IPP TOTAL	PT BIO	Small Hydro	WC1	WC2	Spider BESS	BW BESS	WIND TOTAL	FIRM NB PURCH	FIRM NFLD PURCH	NB/PEI Emerg Assist	NFLD Emerg Assist
1	816	37	29	0	3	1	44	35	37	28	89	62	15	15	27	30	0	30	30	27	0	26	0	28	21	100	0	50	50					
2	788	34	17	0	3	10	43	36	20	28	87	62	15	17	28	30	0	30	30	27	0	26	0	22	22	100	0	50	50					
3	788	16	20	0	3	8	43	35	29	28	85	62	17	17	28	30	0	30	30	28	0	26	0	30	23	100	0	50	50					
4	808	19	32	0	7	7	44	35	35	28	82	62	16	17	28	30	0	30	30	28	0	26	0	29	21	100	0	50	50					
5	814	26	40	0	4	1	45	35	38	28	80	62	17	17	29	30	0	30	30	28	0	26	1	29	19	100	0	50	50					
6	796	37	26	0	3	1	46	35	27	28	78	62	15	17	28	30	0	30	30	28	0	26	1	28	19	100	0	50	50					
7	736	37	15	0	4	0	50	11	14	27	76	62	11	13	27	30	0	30	30	27	0	26	1	26	18	100	0	50	50					
8	650	36	14	0	3	1	40	3	13	5	73	47	2	3	22	30	0	30	30	27	0	26	1	25	17	100	0	50	50					
9	576	37	19	0	3	1	20	3	28	0	66	23	0	0	4	30	0	30	30	27	0	26	1	12	16	100	0	50	50					
10	554	36	18	0	3	1	17	2	32	0	49	25	0	0	0	30	0	30	30	27	0	26	1	12	13	100	0	50	50					
11	440	17	14	0	4	1	18	0	12	0	43	5	1	1	3	30	0	30	30	27	0	26	1	11	7	57	0	50	50					
12	557	12	34	3	4	1	19	0	7	14	24	22	9	9	28	30	0	30	30	27	0	26	1	23	7	98	0	50	50					
13	535	12	15	3	5	2	18	0	14	22	10	8	11	12	28	30	0	30	30	27	0	26	1	25	7	100	0	50	50					
14	560	11	5	6	4	1	21	0	23	26	14	5	16	17	31	30	0	30	30	27	0	26	1	26	8	100	0	50	50					
15	571	12	4	5	3	1	29	0	28	26	25	13	5	5	36	30	0	30	30	27	0	26	1	24	8	100	0	50	50					
16	571	12	4	5	8	1	35	0	30	26	28	17	3	3	36	30	0	30	30	27	0	26	1	23	3	100	0	42	50					
17	500	12	3	5	1	1	34	0	18	26	19	5	4	6	27	30	0	30	30	27	0	26	2	25	1	68	0	50	50					
18	315	12	4	7	0	2	40	0	3	4	10	0	0	0	25	14	0	15	30	25	0	26	2	22	0	22	0	27	26					
19	310	12	1	7	3	1	39	2	1	1	8	0	0	0	26	12	0	11	30	6	0	26	2	23	0	50	0	25	25					
20	353	12	1	8	7	1	30	2	1	1	7	0	0	0	22	13	0	24	30	22	0	26	2	25	1	68	0	25	25					
21	356	12	0	10	13	3	22	2	1	1	4	0	0	0	22	13	0	30	30	27	0	26	2	25	9	24	0	40	41					
22	359	12	1	9	11	5	22	2	1	1	3	0	0	0	22	6	0	30	30	27	0	26	2	24	11	16	0	50	50					
23	422	12	2	11	10	6	22	1	0	20	3	0	4	1	23	31	0	30	30	27	0	26	5	25	15	20	0	50	50					
24	535	12	1	11	7	6	23	0	0	29	3	0	11	10	26	30	0	30	30	27	0	26	12	25	17	94	0	50	50					



Net Thermal Generation

Hour	System Load	PA1	LIN1	LIN2	LIN3	LIN4	TR5	TR6	PT2	TUC1	TUC2	TUC3	TUC4	TUC5	TUC6	BS1	BS2	BS3	BS4	VJ1	VJ2	TK4	IPP Total	PT Bio	Small Hydro	WC1	WC2	Spider BESS	BW BESS	Wind Total	Firm NB Purch	Firm NFDL Purch	NB/PEI Emerg Assist	NFLD Emerg Assist
1	2172	156	149	123	147	142	116	149	154	47	95	128	37	38	19	0	0	0	0	0	0	0	23	15	52	0	0	-47	-39	421	0	199	0	0
2	2140	152	147	121	146	138	116	147	153	47	93	124	37	36	19	0	0	0	0	0	0	0	24	16	50	0	0	-50	-17	408	0	199	0	0
3	2099	164	140	122	146	141	113	146	142	47	85	112	37	36	19	0	0	0	0	0	0	0	24	18	45	0	0	-5	-29	396	0	199	0	0
4	2066	166	121	121	145	142	119	145	129	46	88	114	36	36	19	0	0	0	0	0	0	0	24	17	45	0	0	0	0	389	0	199	0	0
5	2076	154	119	123	149	140	129	144	132	47	85	110	36	36	19	0	0	0	0	0	0	0	24	16	48	0	0	-1	0	403	0	199	0	0
6	2114	161	132	125	150	140	128	146	139	47	85	115	36	36	19	0	0	0	0	0	0	0	24	17	52	0	0	0	-1	384	0	199	0	0
7	2164	158	149	124	150	143	103	145	141	68	91	127	48	48	23	0	0	0	0	0	0	0	24	17	57	24	0	0	0	355	0	199	0	0
8	2241	159	151	126	150	144	81	144	146	76	89	128	48	48	23	4	0	4	0	0	0	0	24	17	56	78	0	-2	-2	355	21	154	0	0
9	2311	159	151	126	152	144	104	144	149	76	96	128	48	48	27	20	0	19	0	13	0	0	24	16	58	74	0	-2	-2	346	21	154	0	0
10	2336	157	151	125	151	144	122	144	149	76	85	116	46	46	42	20	0	16	0	20	0	0	24	16	60	39	0	-9	-9	357	75	154	0	0
11	2320	164	149	126	151	144	123	138	148	76	84	120	48	48	44	2	0	15	0	16	0	0	24	38	59	37	0	-8	-6	338	75	154	0	0
12	2294	171	150	126	151	143	114	151	170	77	77	124	46	46	33	0	0	0	6	17	0	0	24	28	60	76	0	0	0	297	75	154	0	0
13	2263	171	151	127	151	142	106	142	151	47	80	128	44	44	22	0	0	22	21	20	0	0	24	15	65	79	0	0	0	271	75	154	0	0
14	2226	172	151	125	151	143	105	144	152	47	84	128	44	44	21	0	0	24	23	20	0	0	24	15	68	58	0	0	0	244	75	154	0	0
15	2241	172	149	125	151	143	117	146	152	46	97	128	44	44	21	8	0	24	24	20	0	3	24	16	65	77	0	0	0	202	75	154	0	0
16	2300	172	148	124	151	143	120	148	148	49	99	128	45	45	23	26	0	27	27	26	0	26	24	22	72	98	0	0	-2	159	75	154	0	0
17	2387	172	147	124	151	141	135	150	148	74	99	128	48	48	43	30	0	30	30	27	0	5	24	41	79	100	0	12	16	120	70	154	0	100
18	2459	173	148	125	150	145	137	152	151	76	99	128	48	48	45	29	0	30	30	27	0	23	24	41	77	94	0	15	15	92	54	154	28	100
19	2431	173	149	127	152	146	125	153	151	76	99	128	48	48	45	26	0	26	26	27	0	26	24	28	77	61	0	23	23	84	72	154	30	100
20	2384	170	149	126	152	144	124	153	152	76	99	128	48	48	37	24	0	24	24	27	0	24	24	14	76	70	0	28	28	71	47	154	30	100
21	2324	169	150	125	151	137	136	153	152	76	99	128	48	48	33	16	0	18	16	27	0	17	24	15	75	48	0	20	20	74	59	154	30	100
22	2237	169	149	129	153	134	136	154	152	76	99	128	47	47	26	17	0	18	16	27	0	17	24	15	76	49	0	14	14	69	60	154	0	63
23	2129	169	149	131	153	138	126	155	152	64	99	128	34	34	18	20	0	21	23	3	0	22	24	15	78	95	0	0	0	58	64	154	0	0
24	2064	169	149	133	152	135	121	157	152	46	99	128	31	31	17	18	0	19	21	0	0	24	14	61	65	0	0	0	0	54	66	199	0	0

Chart Data

SOLID FUEL	OIL / GAS	NS HYDRO	WIND	IMPORTS	BESS Discharging
1173	364	67	421	199	0
1161	357	66	408	199	0
1156	336	63	396	199	0
1131	339	62	389	199	0
1130	333	64	403	199	0
1162	338	69	384	199	0
1153	404	74	355	199	0
1144	420	74	355	175	0
1170	475	74	346	175	0
1183	467	76	357	229	0
1206	452	97	338	229	0
1200	419	89	297	229	0
1181	428	80	271	229	0
1181	434	82	244	229	0
1194	460	81	202	229	0
1201	521	94	159	229	0
1234	562	120	120	324	28
1246	583	118	92	336	30
1228	575	105	84	356	46
1208	558	90	71	331	56
1213	527	90	74	343	40
1215	516	91	69	277	28
1211	465	93	58	218	0
1205	409	75	54	265	0

Max Net Output: 173 151 133 155 148 137 157 154 76 99 128 48 48 45 30 0 30 30 27 0 26 24 41 79 100 50 50

Remaining Generation Supply / Reserve

Hour	REMAINING SUPPLY /RESERVE	PA1	LIN1	LIN2	LIN3	LIN4	TR5	TR6	PT2	TUC1	TUC2	TUC3	TUC4	TUC5	TUC6	BS1	BS2	BS3	BS4	VJ1	VJ2	TK4	IPP TOTAL	PT BIO	Small Hydro	WC1	WC2	Spider BESS	BW BESS	WIND TOTAL	FIRM NB PURCH	FIRM NFDL PURCH	NB/PEI Emerg Assist	NFLD Emerg Assist
1	550	17	2	10	8	6	21	7	0	29	4	1	11	10	26	30	0	30	30	27	0	26	1	26	27	100	0	50	50					
2	571	21	4	11	8	10	21	10	0	29	6	5	11	12	26	30	0	30	30	27	0	26	0	26	29	100	0	50	50					
3	602	8	11	10	8	7	24	11	12	29	14	16	11	12	26	30	0	30	30	27	0	26	0	24	34	100	0	50	50					
4	624	6	30	11	10	6	18	11	24	30	10	15	12	12	27	30	0	30	30	27	0	26	0	25	34	100	0	50	50					
5	629	19	32	10	6	8	8	12	21	29	14	18	12	12	27	30	0	30	30	27	0	26	0	25	31	100	0	50	50					
6	587	12	19	7	5	8	9	11	15	29	14	13	12	12	27	30	0	30	30	27	0	26	0	24	27	100	0	50	50					
7	501	14	2	9	5	5	34	12	13	8	8	2	0	0	22	30	0	30	30	27	0	26	0	25	22	76	0	50	50					
8	441	14	0	6	4	3	57	12	7	0	9	0	0	0	22	26	0	26	30	27	0	26	0	24	23	22	0	50	50					
9	362	13	0	7	3	3	33	12	5	0	3	0	0	0	18	10	0	11	30	15	0	26	0	25	21	26	0	50	50					
10	391	16	0	7	4	4	15	13	5	0	14	13	2	2	3	9	0	13	30	7	0	26	0	25	19	61	0	50	50					
11	385	9	2	7	3	4	14	19	5	0	15	9	0	0	2	28	0	14	30	12	0	26	0	4	20	63	0	50	50					
12	383	2	2	7	4	4	23	15	3	6	21	5	2	2	13	30	0	30	24	11	0	26	0	13	19	24	0	50	50					
13	385	1	0	5	4	5	31	14	2	28	18	0	4	4	24	30	0	8	9	7	0	26	0	27	14	21	0	50	50					
14	398	1	1	8	4	5	32	12	2	29	15	0	4	4	24	30	0	6	7	7	0	26	0	27	11	42	0	50	50					
15	343	1	3	7	3	5	20	10	2	30	2	0	4	4	24	22	0	5	6	8	0	22	1	25	15	23	0	50	50					
16	247	1	3	8	4	5	17	8	6	26	0	0	3	3	22	3	0	3	3	2	0	0	0	19	7	2	0	50	50					
17	136	1	5	8	4	7	2	6	5	1	0	0	0	0	3	0	0	0	0	1	0	21	1	0	0	0	0	38	34					
18	110	0	4	8	4	3	0	5	3	0	0	0	0	0	1	0	0	0	0	0	0	2	0	0	2	6	0	35	35					
19	151	0	2	6	2	2	13	4	3	0	0	0	0	0	0	4	0	4	4	0	0	0	0	13	2	39	0	27	27					
20	171	3	2	6	3	4	13	4	2	0	0	0	0	0	8	6	0	6	6	1	0	2	0	27	3	30	0	22	22					
21	236	4	1	7	4	11	1	3	2	0	0	0	0	0	12	13	0	12	14	0	0	9	0	26	4	52	0	30	30					
22	254	4	2	4	2	13	1	3	2	0	0	0	1	1	20	13	0	12	14	0	0	9	1	26	3	51	0	36	36					
23	300	4	3	1	2	10	11	2	2	12	0	0	14	14	28	10	0	9	7	24	0	4	0	26	1	15	0	50	50					
24	398	4	2	0	3	12	16	0	2	30	0	0	17	17	29	12	0	11	9	27	0	26	0	28	18	35	0	50	50					